

$$\begin{aligned} \tau_2 = & I_2(\ddot{q}_1 + \dot{q}_2) + m_2 l_1 l_{c2} \sin q_2 \dot{q}_1^2 \\ & + m_2 l_1 l_{c2} \cos q_2 \ddot{q}_1 + m_2 l_{c2}^2 (\ddot{q}_1 + \ddot{q}_2) \\ & + m_2 l_{c2} g \cos(q_1 + q_2) \end{aligned} \quad (a)$$

$$\begin{aligned} \tau_1 = & \tau_2 + m_1 l_{c1}^2 \ddot{q}_1 + m_1 l_{c1} g \cos q_1 + I_1 \ddot{q}_1 \\ & + m_2 l_1^2 \ddot{q}_1 - m_1 l_1 l_{c2} (\dot{q}_1 + \dot{q}_2)^2 \sin q_2 \\ & + m_2 l_1 l_{c2} (\ddot{q}_1 + \ddot{q}_2) \cos q_2 \end{aligned} \quad (b)$$

Control of Robot Manipulator

The majority of robot manipulators in practice are PD control. We start with very simple control. Consider an N-DOF rigid robot manipulator.

$$\ddot{q}^T D(q) + C(q, \dot{q}) \dot{q} + G(q) = \tau$$

$$\tau = \begin{bmatrix} \tau_1 \\ \vdots \\ \tau_n \end{bmatrix} \quad q = \begin{bmatrix} q_1 \\ \vdots \\ q_n \end{bmatrix}$$

$$\text{let } q^d(t) = \begin{bmatrix} q_1^d(t) \\ \vdots \\ q_n^d(t) \end{bmatrix}$$

trajectory (Desired Trajectory)

Design the control input τ such that q is bounded and $\lim_{t \rightarrow \infty} [q(t) - q^d(t)] = 0$

Let us assume that there is some trajectory error.

$$\tilde{q} = q^d - q$$

Assume that the robot parameters are known (i.e. $D(q)$, $C(q, \dot{q})$, $G(q)$ are known)

Computed torque control

let

$$\tau = C(q, \dot{q}) \dot{q} + G(q) + D(q) V \quad (2)$$

V will be designed later.

① & ② together

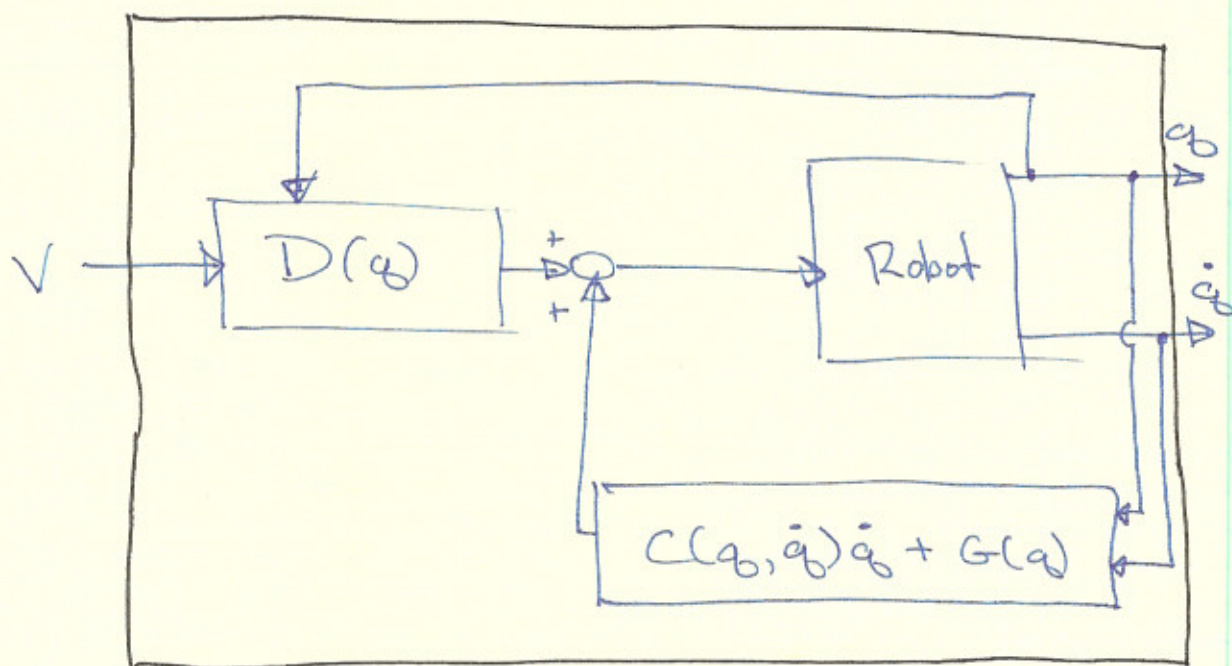
$$D(q) \ddot{q} + C(q, \dot{q}) \dot{q} + G(q)$$

$$= C(q, \dot{q}) \dot{q} + G(q) + D(q) V$$

$$D(q) \ddot{q} = D(q) V$$

Since $\det(D(q)) \neq 0$

$$\ddot{q} = v$$



$$= \frac{1}{s^2}$$

Note: It is not really this easy.

$$\ddot{q} = v$$

$$v = \ddot{q}_d + K_v \dot{\tilde{q}} + K_p \tilde{q}$$

$$K_p = \begin{bmatrix} k_{p1} & & \\ & k_{p2} & \\ & & \ddots \end{bmatrix} \quad K_v = \begin{bmatrix} k_{v1} & & \\ & \ddots & \\ & & k_{vn} \end{bmatrix}$$

$$K_{pi} > 0 \quad K_{vi} > 0$$

$$\dot{c} = 1 \dots n$$

$$\dot{c} = 1 \dots n$$

⑤ & ④

$$\ddot{q}_0 = \ddot{q}_0 + K_v \dot{\tilde{q}}_0 + K_p \tilde{q}_0$$

$$\ddot{\tilde{q}}_0 + K_v \dot{\tilde{q}}_0 + K_p \tilde{q}_0 = 0$$

$$\therefore \ddot{\tilde{q}}_i + K_{vi} \dot{\tilde{q}}_i + K_{pi} \tilde{q}_i = 0$$

$$i = 1 \dots n$$

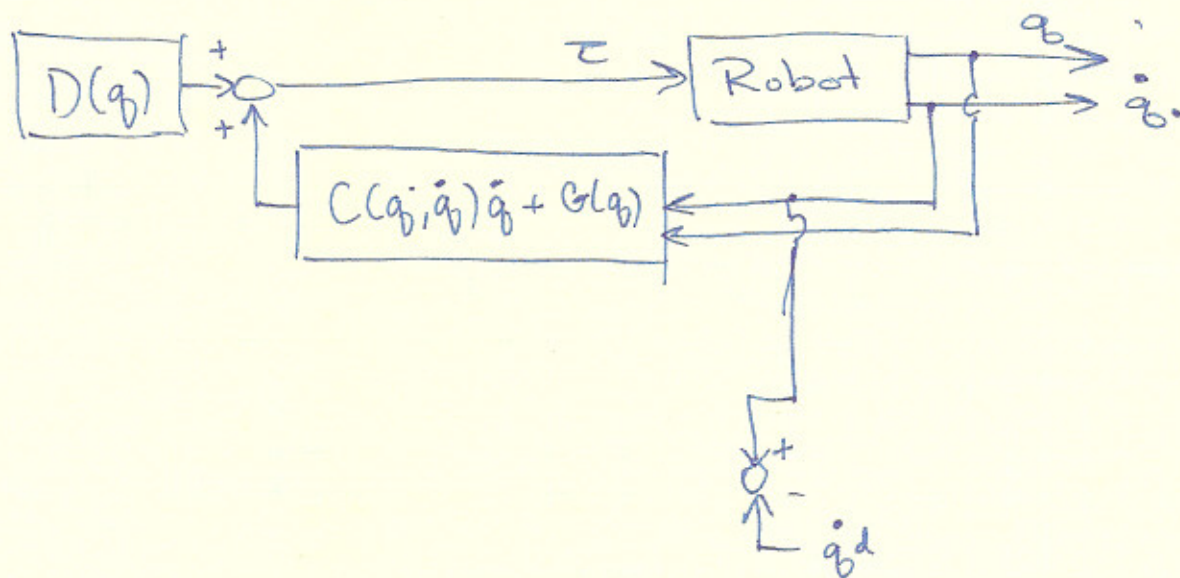
\tilde{q}_i is bounded

$$\lim_{t \rightarrow \infty} \tilde{q}_i(t) = 0$$

When

$$K_{vi} > 0$$

$$K_{pi} > 0$$



PD & gravity Compensation.

$$D(q)\ddot{q} + C(q, \dot{q})\dot{q} + G(q) = \tau$$

this does not consider friction.

this is all we know

$$q_d = \begin{bmatrix} q_1^d \\ \vdots \\ q_n^d \end{bmatrix}$$

desired trajectory
assumed constant.

$$\tilde{q} = q^d - q$$

let $V(q, \dot{q})$ be the Lyapunov function

$$V(\tilde{q}, \dot{\tilde{q}}) = \frac{1}{2} \tilde{q}^T K_P \tilde{q} + \frac{1}{2} \dot{\tilde{q}}^T D(q) \dot{\tilde{q}}$$

This is the energy.

$$V(\tilde{q}, \dot{\tilde{q}}) > 0 \quad (\text{positive definite})$$

$$\dot{V} = \tilde{q}^T K_P \dot{\tilde{q}} + \frac{1}{2} \dot{\tilde{q}}^T D(q) \dot{\tilde{q}}$$

$$+ \frac{1}{2} \dot{\tilde{q}}^T \left[\overbrace{D(q) \dot{\tilde{q}}}^{\cdot} \right]$$

$$= \tilde{q}^T K_P \dot{\tilde{q}} + \frac{1}{2} \dot{\tilde{q}}^T D(q) \dot{\tilde{q}} + \frac{1}{2} \dot{\tilde{q}}^T \left[\dot{D}(q) \dot{\tilde{q}} + D(q) \ddot{\tilde{q}} \right]$$

$$\neq (q^d = \text{constant})$$

$$\dot{\tilde{q}} = \dot{q}^d - \dot{q} = -\dot{q} \quad , \quad \ddot{\tilde{q}} = -\ddot{q}$$

$$\begin{aligned} \dot{V} = \tilde{q}^T K_P \dot{\tilde{q}} + \frac{1}{2} \dot{\tilde{q}}^T D(q) \ddot{\tilde{q}} + \frac{1}{2} \dot{\tilde{q}}^T \dot{D}(q) \dot{\tilde{q}} \\ + \frac{1}{2} \dot{\tilde{q}}^T \dot{D}(q) \dot{\tilde{q}} \end{aligned}$$

$$\dot{V} = \tilde{q}^T K_p \dot{\tilde{q}} - \tilde{q}^T D(q) \ddot{q} + \frac{1}{2} \dot{\tilde{q}}^T D(q) \dot{\tilde{q}}$$

$$D(q) \ddot{q} = -C(q, \dot{q}) \dot{q} - G(q) + \tau$$

then

$$\begin{aligned} \dot{V} &= \tilde{q}^T K_p \dot{\tilde{q}} - \tilde{q}^T [-C(q, \dot{q}) \dot{q} - G(q) + \tau] \\ &\quad + \frac{1}{2} \dot{\tilde{q}}^T \dot{D}(q) \dot{\tilde{q}} \end{aligned}$$

$$\begin{aligned} \dot{V} &= -\tilde{q}^T K_p \dot{\tilde{q}} + \dot{\tilde{q}}^T [-C(q, \dot{q}) \dot{q} - G(q) + \tau] \\ &\quad + \frac{1}{2} \dot{\tilde{q}}^T \dot{D}(q) \dot{\tilde{q}} \end{aligned}$$

$$\begin{aligned} \dot{V} &= -\tilde{q}^T K_p \dot{\tilde{q}} + \dot{\tilde{q}}^T \left[\frac{1}{2} \dot{D}(q) - C(q, \dot{q}) \right] \dot{\tilde{q}} \\ &\quad + \dot{\tilde{q}}^T [-G(q) + \tau] \end{aligned}$$

$$\begin{aligned} \dot{V} &= -\tilde{q}^T K_p \dot{\tilde{q}} + \frac{1}{2} \dot{\tilde{q}}^T [\dot{D}(q) - 2C(q, \dot{q})] \dot{\tilde{q}} \\ &\quad + \dot{\tilde{q}}^T [\tau - G(q)] \end{aligned}$$

$$\dot{V} = -\tilde{q}^T K_p \dot{\tilde{q}} + \dot{\tilde{q}}^T [\tau - G(q)]$$

$$\tau = K_p \tilde{q} - K_D \dot{\tilde{q}} + G(q)$$

$$\dot{V} = -\dot{\tilde{q}}^T K_p \dot{\tilde{q}} \leq 0$$

$$\left. \begin{array}{l} K_D = K_D^T > 0 \\ K_P = K_P^T > 0 \end{array} \right\} \text{Positive definite matrices}$$

$$\dot{V} \rightarrow 0$$

$$\dot{\tilde{q}} \rightarrow 0$$

$$\ddot{\tilde{q}} \rightarrow 0$$

$$\tau = G(q)$$

$$\tau = K_P \tilde{q} + G(q)$$

$$\tilde{q} = 0$$

For industrial design we say $G(q) = 0$

$$\tau = K_P \tilde{q} - K_D \dot{\tilde{q}}$$

$$\tilde{q} \rightarrow \epsilon$$

ϵ becomes small i

$$\tau = K_P \tilde{q} - \frac{K_D}{1 - z^{-1}} [q]$$